

# **LMV321**

# General Purpose, Rail-to-Rail Output Amplifier Rail-to-Rail Amplifiers

#### **FEATURES**

- 130µA supply current
- 1MHz gain bandwidth
- Input voltage range with 5V supply: -0.2V to 4.2V
- Output voltage range with 5V supply: 0.065V to 4.99V
- >1V/µs slew rate
- No crossover distortion
- Fully specified at 2.7V and 5V supplies
- LMV321: Pb-free TSOT-5

#### **APPLICATIONS**

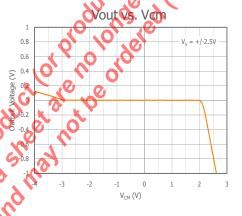
- Portable/battery-powered applications
- Mobile communications, cell phones, pagers
- ADC buffer
- Active filters
- Portable test instruments
- Signal conditioning
- Medical Equipment
- Portable medical instrumentation

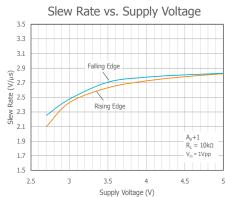
## **General Description**

The LMV321 is a single channel, low cost, voltage feedback amplifier. The LMV321 consumes only  $130\mu\text{A}$  of supply current and is designed to operate from a supply range of 2.7V to 5.5V ( $\pm1.35$  to  $\pm2.75$ ). The input voltage range extends 200mV below the negative rational 800mV below the positive rail.

The LMV321 is fabricated on a CMOS process. It offers 1MHz gain bandwidth product and  $>1V/\mu s$  slew rate. The combination of low power, low supply voltage operation, and rail-to-fail performance make the LMV321 well suited for battery-powered systems. The LMV321 is packaged in the space saving TSOT-5 package. TSOT-5 package is pin compatible with the SOT23-5 package.

## Typical Performance Examples



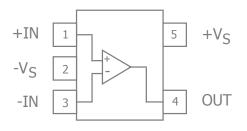


## **Ordering Information**

Part Number	Package	Pb-Free	RoHS Compliant	Operating Temperature Range	Packaging Method
LMV321IST5X	TSOT-5	Yes	Yes	-40°C to +85°C	Reel

Moisture sensitivity level for all parts is MSL-1.

## LMV321 Pin Configuration



## LMV321 Pin Assignments<sup>1</sup>

Pin No.	Pin Name	Description
1	+IN	Positive input
2	-V <sub>S</sub>	Negative supply
3	-IN	Negative input
4	OUT	Output
5	+V <sub>S</sub>	Positive supply

#### Notes:

1.Pin compatible to SOT23-5.

The product are no ordered (OBS)

## **Absolute Maximum Ratings**

The safety of the device is not guaranteed when it is operated above the "Absolute Maximum Ratings". The device should not be operated at these "absolute" limits. Adhere to the "Recommended Operating Conditions" for proper device function. The information contained in the Electrical Characteristics tables and Typical Performance plots reflect the operating conditions noted on the tables and plots.

Parameter	Min	Max	Unit		
Supply Voltage		7	V		
Input Voltage Range	-V <sub>S</sub> -0.4V	+V <sub>S</sub>	V		
Continuous Output Current	Output is protected against momentary short circuit				

## **Reliability Information**

Parameter	Min	Тур	Max	Unit		
Junction Temperature			150	°C		
Storage Temperature Range	-65	17.	150	°C		
Lead Temperature (Soldering, 10s)			260	°C		
Package Thermal Resistance						
5-Lead TSOT		221		°C/W		

## **ESD Protection**

Product	TSOT-5
Human Body Model (HBM)	2kV
Charged Device Model (CDM)	2kV

## **Recommended Operating Conditions**

Lead Temperature (Soldering, 103)				200	C
Package Thermal Resistance			0 60		
5-Lead TSOT		221		°C/W	
Notes: Package thermal resistance $(\theta_{JA}),$ JDEC standard, mu	lti-layer test boards, still air.	anti	Mal		
ESD Protection		We !!	O		
Product	TSOT-5	's 'no'	BS		
Human Body Model (HBM)	2kV		)*		
Charged Device Model (CDM)	2kV	'd h	•		
Recommended Operating Cond Parameter	itions	Min	Тур	Max	Unit
Operating Temperature Range	100	-40	- 7 F	+85	°C
Supply Voltage Range	110, 8, 40	2.7		5.5	V
	and may not				

## Electrical Characteristics at +2.7V

 $T_A=25$  °C,  $V_S=+2.7$ V,  $R_f=R_g=10$  K $\Omega$ ,  $R_L=10$ k $\Omega$  to  $V_S/2$ , G=2; unless otherwise noted.

Parameter	Conditions	Min	Тур	Max	Units
nce					
Input Offset Voltage			1.7	7	mV
Average Drift			5		μV/°C
Input Bias Current			<1	250	nA
Input Offset Current			<1	50	nA
Common Mode Rejection Ratio	$0V \le V_{CM} \le 1.7V$	50	63		dB
Power Supply Rejection Ratio	$2.7V \le V^{+} \le 5V, V_{O}=1V, V_{CM}=1V$	50	60		dB
Common Mode Input Range	For V <sub>CM</sub> ≤ 50 dB	0	-0.2		V
				1.7	V
Output Voltage Swing	$R_L = 10k\Omega \text{ to } V_S/2$	V+-100			mV
		100	60		mV
Supply Current			110	170	μΑ
nce		C			1
Gain Bandwidth Product	C <sub>L</sub> =200 pF	•	1		MHz
Phase Margin	ye yu		60		0
Gain Margin	10, 91		10		dB
Input Voltage Noise	f = 1kHz		46		nV/√Hz
	aroductiver LOV				
	Average Drift Input Bias Current Input Offset Current Common Mode Rejection Ratio Power Supply Rejection Ratio Common Mode Input Range	Average Drift  Input Bias Current  Input Offset Current  Common Mode Rejection Ratio $0V \le V_{CM} \le 1.7V$ Power Supply Rejection Ratio $2.7V \le V^+ \le 5V$ , $V_O = 1V$ , $V_{CM} = 1V$ Common Mode Input Range  For $V_{CM} \le 50$ dB	Average Drift Input Bias Current Input Offset Current Common Mode Rejection Ratio $0V \le V_{CM} \le 1.7V$ 50 Power Supply Rejection Ratio $2.7V \le V^+ \le 5V, V_0 = 1V, V_{CM} = 1V$ 50 Common Mode Input Range For $V_{CM} \le 50 \text{ dB}$ 0 Output Voltage Swing $R_L = 10k\Omega \text{ to } V_S/2$ $Supply Current$ Gain Bandwidth Product $C_L = 200 \text{ pF}$ Phase Margin Gain Margin Input Voltage Noise $f = 1k\text{Hz}$	Average Drift 5 Input Bias Current	Average Drift       5         Input Bias Current       <1

#### Notes:

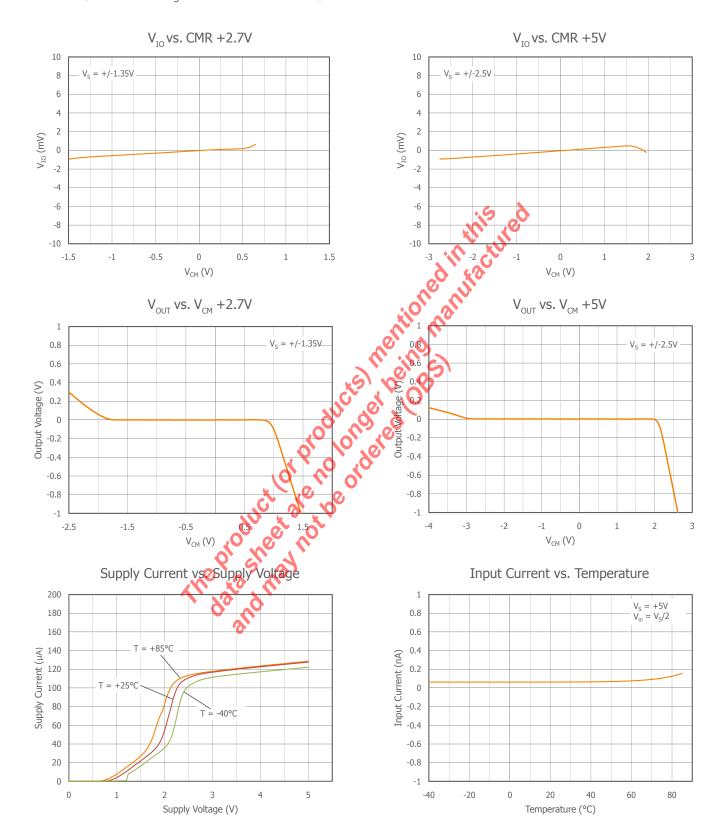
## Electrical Characteristics at +5V

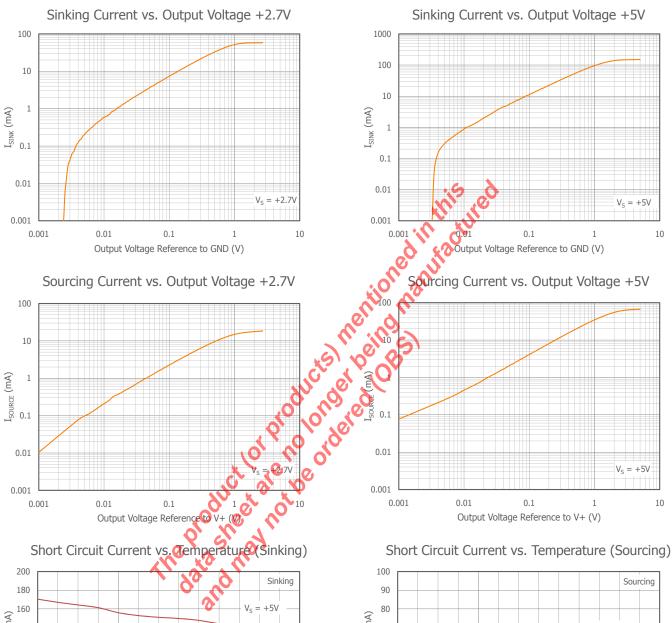
 $T_A=25$ °C,  $V_S=+5V$ ,  $R_f=R_g=10k\Omega$ ,  $R_L=10k\Omega$  to  $V_S/2$ , G=2; unless otherwise noted. **Boldface** limits apply at the temperature extremes.

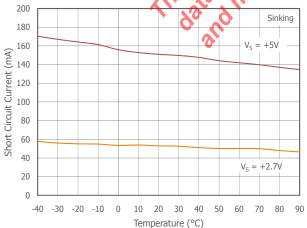
Symbol	Parameter	Conditions	Min	Тур	Max	Units
DC Performa	ince	'				
V <sub>IO</sub>	Input Offset Voltage			1.7	7 <b>9</b>	mV
dV <sub>IO</sub>	Average Drift			5		μV/°C
I <sub>b</sub>	Input Bias Current			<1	250 <b>500</b>	nA
I <sub>OS</sub>	Input Offset Current			<1	50 <b>150</b>	nA
CMRR	Common Mode Rejection Ratio	$0V \le V_{CM} \le 4V$	50	65		dB
PSRR	Power Supply Rejection Ratio	$2.7V \le V^+ \le 5V$ , $V_0 = 1V$ , $V_{CM} = 1V$	.6 50	60		dB
CMIR	Common Mode Input Range	For V <sub>CM</sub> ≤ 50 dB	0 0	-0.2		V
			, 10,	4.2	4	V
A <sub>OL</sub>	Open-Loop Gain	$R_L = 2k\Omega$	15 10	100		V/mV
V <sub>OUT</sub> Output Voltage Swing	$2.7V \le V^+ \le 5V, V_O = 1V, V_{CM} = 1V$ For $V_{CM} \le 50 \text{ dB}$ $R_L = 2k\Omega$ $R_L = 2k\Omega \text{ to } V_S / 2$ $R_L = 10k\Omega \text{ to } V_S / 2$ Sourcing $V_O = 0V$	V+-300 <b>V+-400</b>	V+-40		mV	
		sent diff		120	300 <b>400</b>	mV
		$R_L = 10k\Omega \text{ to } V_S \Omega$	V+-100 <b>V+-200</b>	V+-10		mV
		Auction (Or		65	180 <b>280</b>	mV
$I_{SC}$	Short Circuit Output Current	Sourcing V <sub>0</sub> = 0V	5	60		mA
		Sinking V <sub>0</sub> =5V	10	160		mA
$I_S$	Supply Current	(of no order		130	250 <b>350</b>	μА
AC Perform	ance	CL 10 0				
SR	Slew Rate	, O , V		>1		V/µs
GBWP	Gain Bandwidth Product	€ C € 200 pF		1		MHz
Φ <sub>m</sub>	Phase Margin	10 K		60		0
G <sub>m</sub>	Gain Margin	€ C €200 pF		10		dB
e <sub>n</sub>	Input Voltage Noise	f = 1kHz		39		nV/√Hz

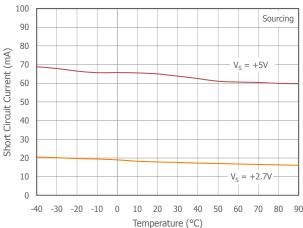
#### Notes:

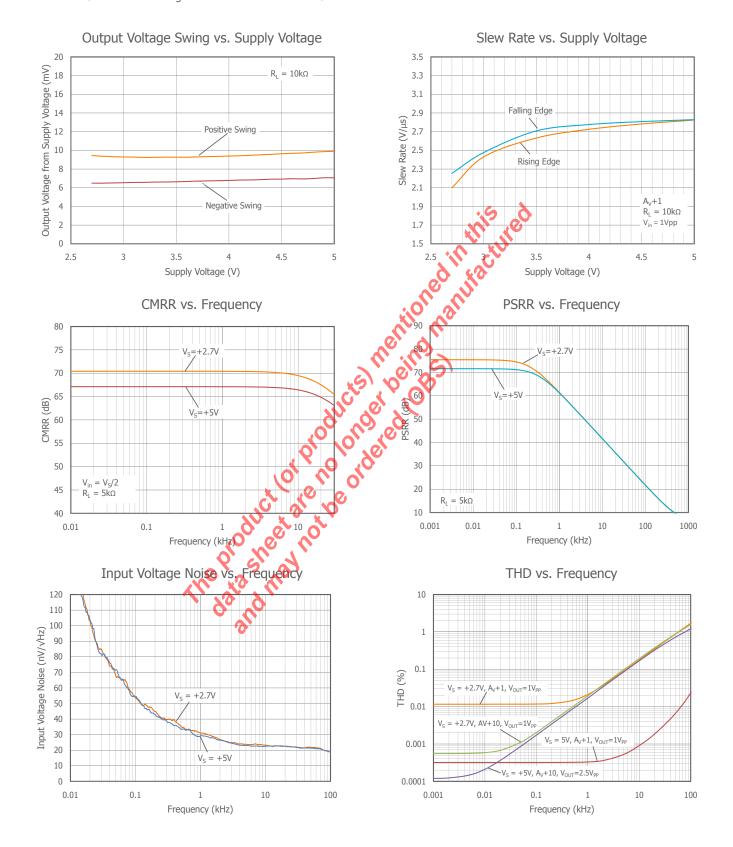
Min max specifications are guaranteed by testing, design, or characterization

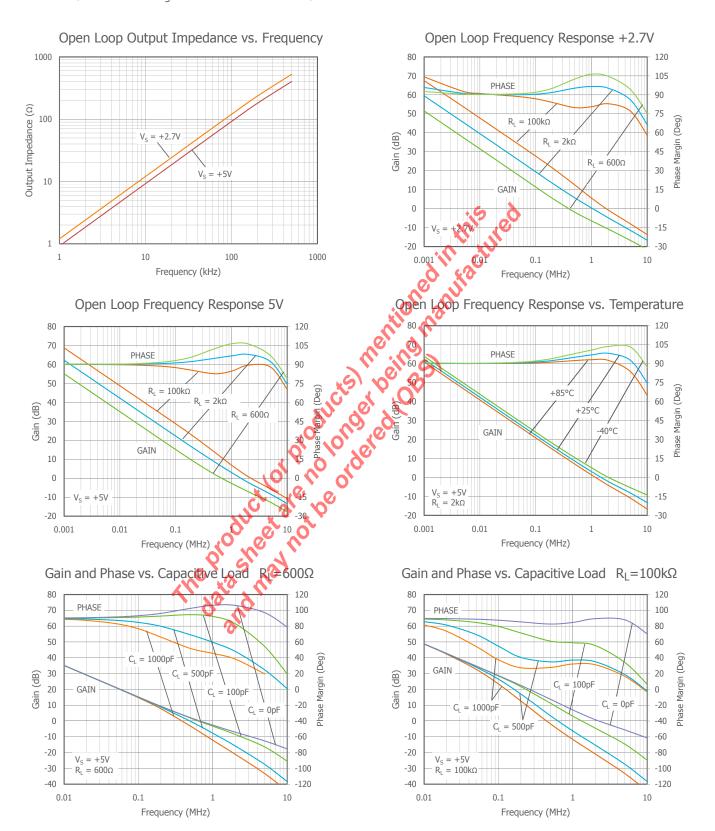


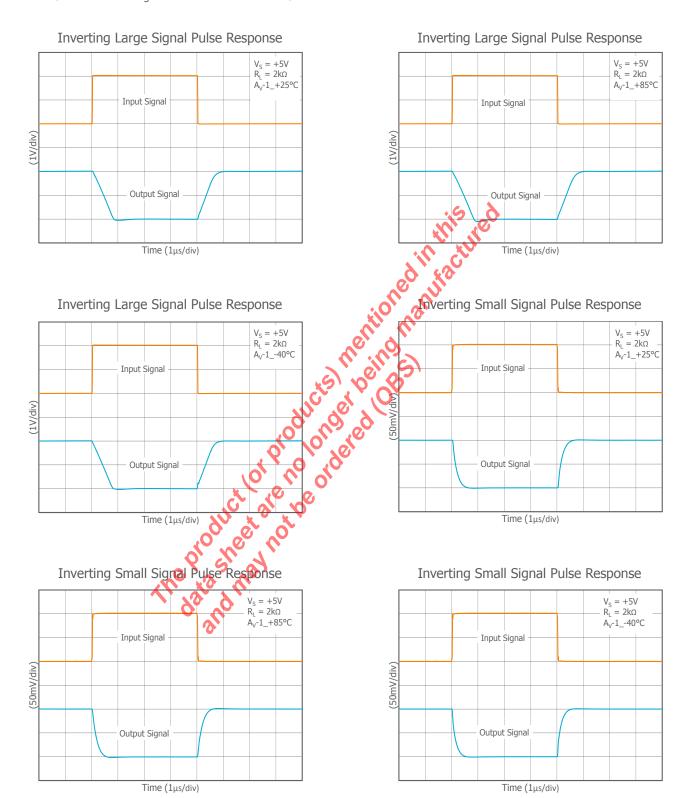






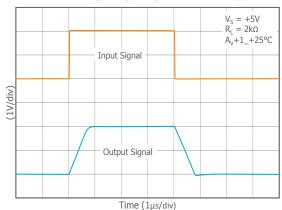




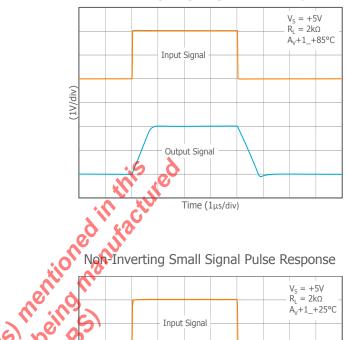


 $T_A = 25$ °C,  $V_S = +5V$ ,  $R_f = R_q = 10k\Omega$ ,  $R_L = 10k\Omega$  to  $V_S/2$ , G = 2; unless otherwise noted.

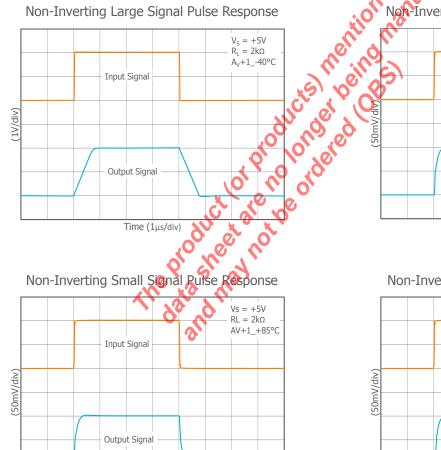


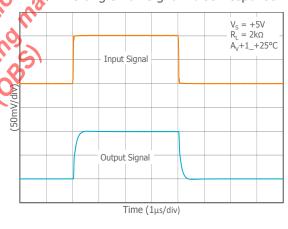


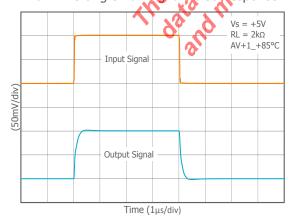
## Non-Inverting Large Signal Pulse Response



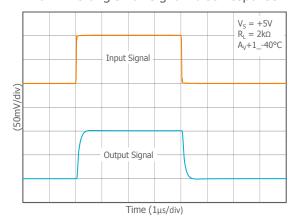
#### Non-Inverting Large Signal Pulse Response







#### Non-Inverting Small Signal Pulse Response



## **Application Information**

#### **General Description**

The LMV321 is a single supply, general purpose, voltagefeedback amplifier fabricated on a CMOS process. The LMV321 offers 1MHz gain bandwidth product, >1V/µs slew rate, and only 130µA supply current. It features a rail-to-rail output stage and is unity gain stable.

The common mode input range extends to 200mV below ground and to 800mV below Vs. Exceeding these values will not cause phase reversal. However, if the input voltage exceeds the rails by more than 0.5V, the input ESD devices will begin to conduct. The output will stay at the rail during this overdrive condition.

The output stage is short circuit protected and offers "soft" saturation protection that improves recovery time. Figures 1, 2, and 3 illustrate typical circuit configurations for noninverting, inverting, and unity gain topologies for dual supply applications. They show the recommended bypass capacitor values and overall closed loop gain equations. Figure 4 shows the typical non-inverting gain circuit for single supply applications



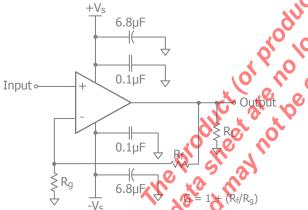


Figure 1. Typical Non-Inverting Gain Circuit

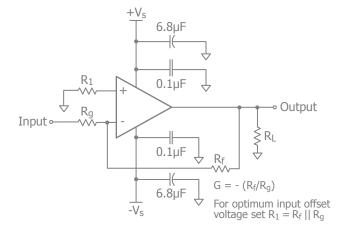


Figure 2. Typical Inverting Gain Circuit

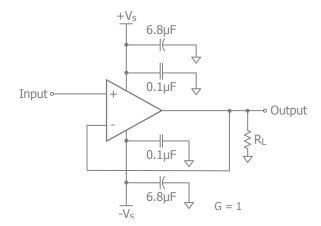


Figure 3. Unity Gain Circuit

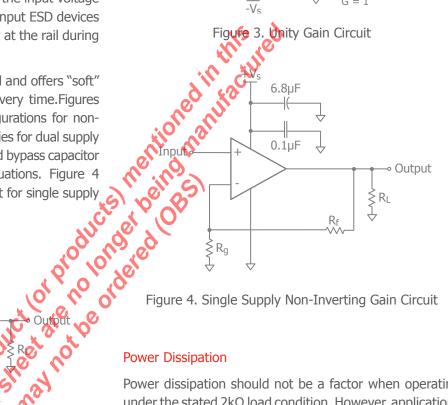


Figure 4. Single Supply Non-Inverting Gain Circuit

Power dissipation should not be a factor when operating under the stated  $2k\Omega$  load condition. However, applications with low impedance, DC coupled loads should be analyzed to ensure that maximum allowed junction temperature is not exceeded. Guidelines listed below can be used to verify that the particular application will not cause the device to operate beyond it's intended operating range.

Maximum power levels are set by the absolute maximum junction rating of 150°C. To calculate the junction temperature, the package thermal resistance value Theta<sub>1A</sub>  $(\Theta_{1A})$  is used along with the total die power dissipation.

$$T_{1unction} = T_{Ambient} + (\Theta_{1A} \times P_{D})$$

Where T<sub>Ambient</sub> is the temperature of the working environment.

In order to determine P<sub>D</sub>, the power dissipated in the load needs to be subtracted from the total power delivered by the supplies.

$$P_D = P_{supply} - P_{load}$$

Supply power is calculated by the standard power equation.

$$P_{\text{supply}} = V_{\text{supply}} \times I_{\text{RMS supply}}$$

$$V_{\text{supply}} = V_{S+} - V_{S-}$$

Power delivered to a purely resistive load is:

$$P_{load} = ((V_{l OAD})_{RMS^2})/Rload_{eff}$$

The effective load resistor (Rloadeff) will need to include the effect of the feedback network. For instance,

Rloadeff in Figure 3 would be calculated as:

$$R_L \mid\mid (R_f + R_g)$$

These measurements are basic and are relatively easy to perform with standard lab equipment. For design purposes however, prior knowledge of actual signal levels and load impedance is needed to determine the dissipated power. Here, PD can be found from

$$P_D = P_{Quiescent} + P_{Dynamic} - P_{Load}$$

Quiescent power can be derived from the specified 19 values along with known supply voltage, V<sub>Supply</sub> load power can be calculated as above with the desired signal amplitudes using:

$$(V_{1} \cap AD)_{PMS} = V_{PEAK} / \sqrt{2}$$

$$(V_{LOAD})_{RMS} = V_{PEAK} / \sqrt{2}$$
  
(  $I_{LOAD})_{RMS} = (V_{LOAD})_{RMS} / Ripad_{eff}$ 

The dynamic power is focused primarily within the output stage driving the load. This value can be calculated as:

Assuming the load is referenced in the middle of the power rails or V<sub>supply</sub>/2.

The LMV321 is short circuit protected. However, this may not guarantee that the maximum junction temperature (+150°C) is not exceeded under all conditions.

### **Driving Capacitive Loads**

Increased phase delay at the output due to capacitive loading can cause ringing, peaking in the frequency response, and possible unstable behavior. Use a series resistance, RS, between the amplifier and the load to help improve stability and settling performance. Refer to Figure 5.

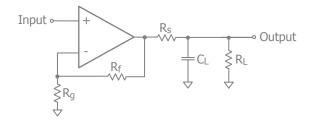


Figure 5. Addition of R<sub>S</sub> for Driving Capacitive Loads

For a given load capacitance, adjust R<sub>S</sub> to optimize the tradeoff between settling time and bandwidth. In general, reducing R<sub>S</sub> will increase bandwidth at the expense of additional overshoot and ringing.

## Overdrive Recovery

An overdrive condition is defined as the point when either one of the inputs or the output exceed their specified voltage range. Overdrive recovery is the time needed for the amplifier to return to its normal or linear operating point. The recovery time varies, based on whether the inputor output is overdriven and by how much the range is exceeded. The LMV321 and will typically recover in less than bus from an overdrive condition. Figure 6 shows the LMY321 in an overdriven condition.

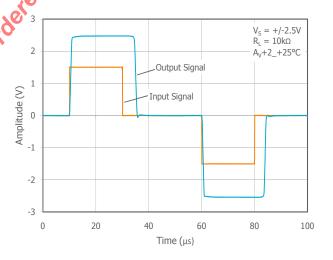


Figure 6. Overdrive Recovery

#### **Layout Considerations**

General layout and supply bypassing play major roles in high frequency performance. CADEKA has evaluation boards to use as a guide for high frequency layout and as an aid in device testing and characterization. Follow the steps below as a basis for high frequency layout:

■ Include 6.8µF and 0.1µF ceramic capacitors for power

supply decoupling

- Place the 6.8µF capacitor within 0.75 inches of the power pin
- Place the 0.1µF capacitor within 0.1 inches of the power pin
- Remove the ground plane under and around the part, especially near the input and output pins to reduce parasitic capacitance
- Minimize all trace lengths to reduce series inductances

#### **Evaluation Board Schematics**

Evaluation board schematics and layouts are shown in Figures 7-9. These evaluation boards are built for dual supply operation. Follow these steps to use the board in a single-supply application:

1. Short -Vs to ground.

2. Use C3 (6.8uF) and C4 (0.1uF), if the -VS pin of the amplifier is not directly connected to the ground plane.

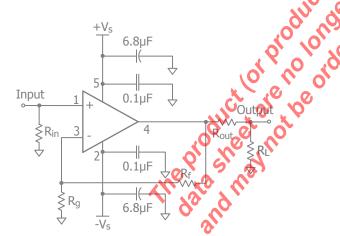


Figure 7. CEB004 Schematic

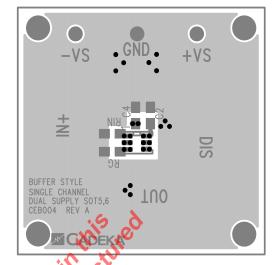


Figure 8. CEB004 Top View

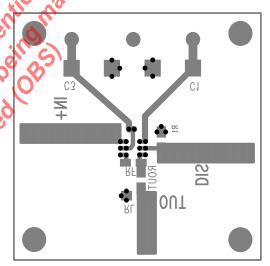
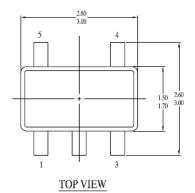


Figure 9. CEB004 Bottom View

#### **Mechanical Dimensions**

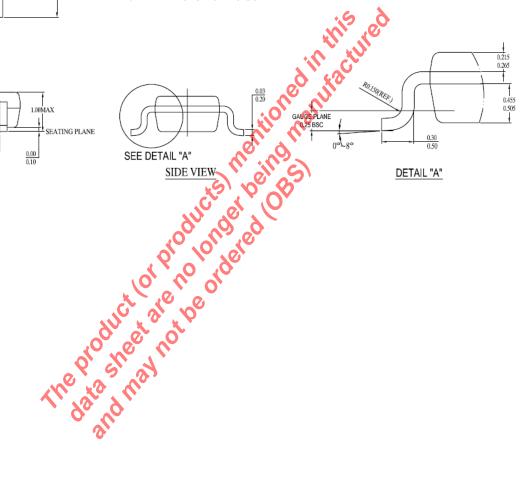
TSOT-5 Package



## 0.34 0.90 0.50 0.50 1.00MAX 1.00MAX SEATING PLANE

#### NOTE:

- 1. ALL DIMENSIONS ARE IN MILLIMETERS.
- 2. PACKAGE LENGTH DOES NOT INCLUDE INTERLEAD FALSH OR PROTRUSION
- 3. PACKAGE WIDTH DOES NOTINCLUDE INTERLEAD FALSH OR PROTRUSION.
- 4. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.10 MILLIMETERS MAX.
- 5. DRAWING CONFROMS TO JEDEC MO-193, VARIATION AA.
- 6. DRAWING IS NOT TO SCALE.



### For Further Assistance:

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